

## Flim Bulk Acoustic-Wave Resonator (FBAR)

Piezoelectric thin films convert electrical energy into mechanical energy and vice versa. Film Bulk Acoustic Resonator (FBAR) consists of a piezoelectric thin film sandwiched by two metal layers. A resonance condition occurs if the thickness of piezoelectric thin film (d) is equal to an integer multiple of a half of the wavelength ( $\lambda_{res}$ ). The fundamental resonant frequency ( $F_{res}=1/\lambda_{res}$ ) is then inversely proportional to the thickness of the piezoelectric material used, and is equal to  $V_a/2d$  where  $V_a$  is an acoustic velocity at the resonant frequency (Fig. 1).

Research

Area

FBAR



Fig. 1 Schematic of longitudinal wave generation and propagation in an acoustic resonator by an electric field in the thickness direction

A bulk-micromachined FBAR with Thickness Field Excitation (Error! Reference source not found.) uses a z-directed electric field to generate z-propagating longitudinal or compressive wave. In an LFE-FBAR, the applied electric field is in y-direction, and the shear acoustic wave (excited by the lateral electric field) propagates in z-direction, as illustrated in Error! Reference source not found ..



Fig. 3 (a) Diagram and (b) a typical implementation of LFE-FBAR

Both TFE-FBAR and LFE-FBAR can equivalent be represented with the equivalent circuit, shown in **Fig.**, called Butterworth-Van Dyke (BVD) circuit. The resonator is modeled by a constant "clamped" capacitance  $C_0$  in parallel with an acoustic or "motional" arm that consists of motional capacitance C<sub>m</sub>, motional inductance L<sub>m</sub>, and motional resistance  $R_m$ . The  $C_o$  is the electrical capacitance between the two electrodes through which the electric field is applied. The motional components (C<sub>m</sub>, L<sub>m</sub> and R<sub>m</sub>) model electromechanical response of a piezoelectric material.



Fig. 4 Butterworth-Van Dyke (BVD) equivalent circuit for a piezoelectric crystal.

The resonant frequency of a TFE FBAR can be tuned by removing a portion of the resonator support layer as shown in Fig. . The removal of the support layer reduces the mass loading effect of the resonator, and increases the resonant frequency.



Fig. 5 Schematic of the post-processing RIE tuning technique which removes the supporting nitride membrane from the backside of a completely processed and tested FBAR.

Both of the resonant frequencies are measured to vary as the mass loading changes. When the  $0.9\mu$ m thick  $Si_3N_4$  support layer is removed by Reactive Ion Etching from the FBAR backside, the resonant frequency of the FBAR increases from 1.1 to 1.5 GHz, around 40% shift. In **Fig. 6**, we show the resonant frequency dependence on the  $Si_3N_4$  support layer thickness measured on three FBARs. A similar experiment has been performed on an FBAR with parylene as its support layer, and the results are shown in **Fig. 7**. As can be seen by comparing **Figs. 6** and **7**, parylene has a much smaller mass loading effect on the frequency shift than  $Si_3N_4$ . This is due to the fact that  $Si_3N_4$  has a larger mass density and much higher Young's Modulus than parylene, and affects the FBAR resonant frequency much more strongly.



Fig. 6 Dependence of series resonant frequency and parallel resonant frequency on the  $Si_3N_4$  thickness.





*Fig.* 7 Series resonant frequency vs. parylene thickness.

**Fig. 8** Electromechanical coupling constant vs.  $Si_3N_4$  thickness (i.e., mass loading).

Electromechanical coupling constant  $k_t^2$  is related to the difference of the two resonant frequencies as

$$k_t^2 = \frac{\pi^2(f_p - f_s)}{4f_s}$$

 $k_t^2$  increases as the Si<sub>3</sub>N<sub>4</sub> is removed from the FBAR backside. The change of  $k_t^2$  as a function of the mass loading by the Si<sub>3</sub>N<sub>4</sub> support layer are plotted in **Fig. 8**, respectively.

An air-backed, Al/ZnO/Al film-bulk-acoustic resonator (FBAR) that is free-standing by itself has been fabricated. Unlike a conventional FBAR structure, the newly fabricated resonator doesn't employ any supporting layer below or above it, but the whole resonator body (consisting of ZnO piezoelectric layer sandwiched by two aluminum layers) suspends by itself in the air. Some SEM pictures of the fabricated FBAR devices with various shapes are shown in **Fig. 9**. **Figure 10** shows SEM picture of the Al bridges that act as leading electrodes and also to hold the FBAR (which free stands in air). Picture of an FBAR viewed from its backside is shown in **Fig. 11**.



Fig. 9 SEM pictures of the fabricated free-standing air-backed FBARs held by Al bridges.



Fig. 10 SEM picture of the 0.3 µm

thick Al bridge.

**Fig. 11** Backside view of an air-backed FBAR.

 $S_{11}$  measurements of an FBAR with its underneath  $Si_3N_4$  layer at 0.9µm, 0.6µm, 0.3µm, 0µm and in the case of the ZnO being patterned from the wafer backside are shown in Fig. 12.



**Fig. 12**  $S_{11}$  of an FBAR when (a)  $Si_3N_4$  thickness is  $0.9\mu m$  (1100MHz~1250MHz) (b)  $Si_3N_4$  thickness is  $0.6\mu m$  (1200MHz~1350MHz) (c)  $Si_3N_4$  thickness is  $0.3\mu m$  (1300MHz~1450MHz) (d)  $Si_3N_4$  is completely removed (1500MHz~1650MHz) (e) ZnO is patterned from backside (1500MHz~1600MHz)

The quality factor  $Q_s$  at the series resonant frequency in the free-standing air-backed FBAR is calculated to be 1,322. It is about six times larger than that in the FBAR with 0.9µm thick Si<sub>3</sub>N<sub>4</sub> as a support diaphragm. The quality factor  $Q_p$  at the parallel resonant frequency in the case (e) is calculated to be 513, three times that in the case (a). Figure of Merit (FOM) of an FBAR is defined as the product of Q and  $k_t^2$ . Insertion loss in an FBAR-based filter is inversely proportional to the FOM of the FBARs. In the free-standing air-backed FBAR, we have increased  $k_t^2$  twice and the quality factor six times, and filters made out of this kind of resonator are expected to have larger bandwidth and much lower insertion loss compared to that made by an FBAR built on a support diaphragm